



## Use of Light Structural Materials (Foam Blocks) in the Construction of Residential Buildings

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**Abstract:** The use of materials with a thin layer of air in external barrier constructions dramatically increases the thermal and technical properties of the wall. Therefore, the heat transfer of an air layer is different from the heat transfer of a solid, solid layer. The thermal resistance of a solid layer is directly proportional to its thickness, the amount of heat passing through the layer is inversely proportional to its thickness.

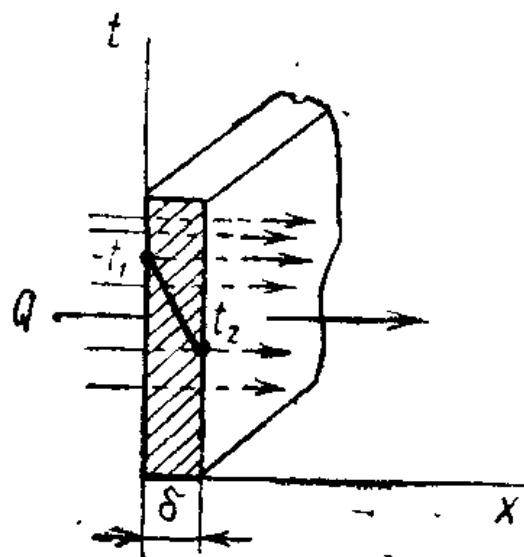
**Keywords:** External barrier construction, heat insulation, glass wool, heat flow density, isothermal surface, straight line equation.

We assume that the heat transfer coefficient of the material does not depend on the temperature. Temperatures on the outer surfaces of the wall are kept constant  $t_1 > t_2$ ; the temperature changes only in the  $x$  direction, which is perpendicular to the wall surface, that is, the temperature field is one-dimensional, the temperature gradient is equal to  $dt/dx$ . We find the density of the heat flow passing through the wall and determine the description of the temperature change according to the wall thickness. Inside the wall, we distinguish an elementary layer with a thickness  $dx$ , bounded by two isothermal surfaces. The Fourier equation for this layer has the following form:

$$q = -\lambda \frac{dt}{dx} \quad (1)$$

Or:

$$dt = -\frac{q}{\lambda} dx \text{ and } t = -\frac{q}{\lambda} dx + c$$



**Figure 1. A flat single-layer wall.**



The integration constant C is determined from the boundary conditions: t=t1 when x=0. From this, C=t1, so the equation will look like this:

$$t = -\frac{q}{\lambda}x + t_1$$

From this equation, it is possible to determine the density of the heat flow passing through the considered wall. If we put the value x=□ into this equation, we get t=t2, from this:

$$q = \frac{\lambda}{\delta}(t_1 - t_2) = \frac{\lambda}{\delta}\Delta t \quad (2)$$

The heat flow density on a flat wall is directly proportional to the heat transfer coefficient  $\lambda$ , temperature difference (t1-t2) and inversely proportional to the wall thickness □. It should be noted that the heat flow is determined not by the absolute value of the temperature, but by their difference - heat pressure  $t_1 - t_2 = \square t$ . The ratio  $l/\square$  is called the thermal conductivity of the wall; its size [W/(m $\square$ grad)]. Equation (3) can be written in a different form:

$$q = \frac{t_1 - t_2}{\delta/\lambda} \quad (3)$$

The heat flow density on a flat wall is directly proportional to the heat transfer coefficient l, temperature difference (t1-t2) and inversely proportional to the wall thickness □. It should be noted that the heat flow is determined not by the absolute value of the temperature, but by their difference - heat pressure  $t_1 - t_2 = \square t$ . The ratio  $l/\square$  is called the thermal conductivity of the wall; its size [W/(m $\square$ grad)]. Equation (3) can be written in a different form:

$$Q = qF\tau = \frac{\delta}{\lambda}\Delta tF\tau \quad (4)$$

If we add the value of q from formula (3) to formula (2), we can get the equation of the temperature curve.

$$t = t_1 - \frac{\Delta t}{\delta}x \quad (5)$$

This equation is called the equation of a straight line. Thus, when the value of  $\lambda$  does not change, the temperature changes linearly along the thickness of the homogeneous wall. For the air layer, such proportionality does not exist. In a solid material, heat transfer is carried out only by heat conduction, and in the air layer, heat is transferred again by means of convection and radiation. Heat flow in external barrier structures depends on the parallel and perpendicular arrangement of pores. If we take into account these factors, the calculation becomes complicated. In practical calculations, assuming that the material consists of pores, the average heat transfer coefficient of the pores is determined.

Let the pores in the foam concrete block be parallel to the heat flow. We determine the thermal resistance of heat transfer using the following formula:

$$R = \frac{F_1 + F_2 + F_3 + \dots}{\frac{F_1}{R_1} + \frac{F_2}{R_2} + \frac{F_3}{R_3} + \dots}$$

Here:



$R_1, R_2, R_3$

– thermal resistance of separate elements of the barrier;

$F_1, F_2, F_3$  are surfaces of individual elements.

The average value of the heat transfer coefficient:

$$\lambda_{oort} = \frac{\lambda_1 \cdot F_1 + \lambda_2 \cdot F_2 + \lambda_3 \cdot F_3 + \dots}{F_1 + F_2 + F_3 + \dots}$$

Here:  $\lambda_1, \lambda_2, \lambda_3$  is the heat transfer coefficient of individual elements of the layer. The density of foam concrete is  $1000 \text{ kg/m}^3$  and the thermal conductivity coefficient is equal to  $\lambda = 0.41 \text{ W/m}\cdot\text{K}$ . According to QMQ 2.01.04-97, if the thickness is 16 mm, it is equal to  $R = 0.136 \text{ m}^2 \cdot \text{OS/W}$ . Considering that the foam concrete is located symmetrically with respect to the central axis, and that the structure of the foam concrete is the same in height, as a calculation surface we take the half width of foam concrete, that is, 95mm.

For surfaces parallel to the heat flow:

Plot 1:

$$R = \frac{0,40}{0,41} = 0,975 \text{ m}^2 \cdot {}^\circ\text{S/Vt}, \quad F_1 = 15 \text{ mm}^2$$

Area 2 16-cell foam concrete:

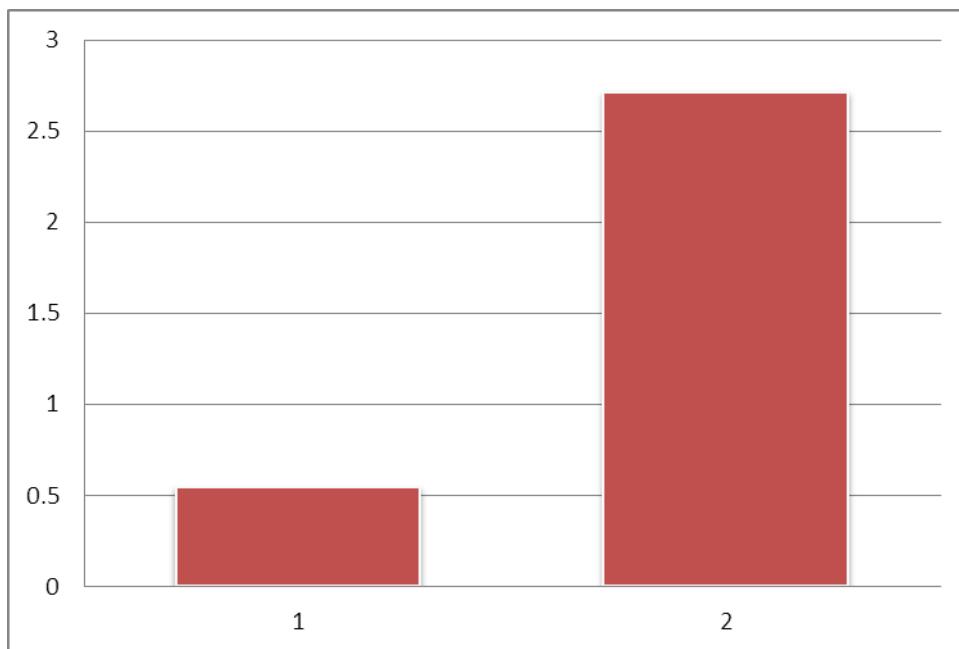
$$R = \frac{0,144}{0,41} + 0,136 \cdot 16 = 2,527 \text{ m}^2 \cdot {}^\circ\text{S/Vt}, \quad F_2 = 60 \text{ mm}^2$$

3rd plot. 8-cell foam concrete:

$$R = \frac{0,272}{0,41} + 0,136 \cdot 8 = 1,75 \text{ m}^2 \cdot {}^\circ\text{S/Vt}, \quad F_3 = 2060 \text{ mm}^2$$

Thermal resistance of foam concrete:

$$R_{\text{tot}} = \frac{15 + 60 + 20}{\frac{15}{0,975} + \frac{60}{2,527} + \frac{20}{1,75}} = 1,88 \text{ m}^2 \cdot {}^\circ\text{S/Vt}$$



1. For surfaces perpendicular to the heat flow:

$$R = (0,0165:0,41) \cdot 2 + (0,0074:0,41) \cdot 15 = 0,35 \text{ m}^2 \cdot {}^\circ\text{S}/\text{Vt}$$

The equivalent coefficient of thermal conductivity for 16-cell foam concrete:

$$\lambda_{ekv} = \frac{\delta}{R} = \frac{0,016}{0,136} = 0,117 \text{ Vt/m} \cdot {}^\circ\text{S}$$

The average heat transfer coefficient of the layer:

$$\lambda_{oirt} = \frac{0,41 \cdot 35 + 0,117 \cdot 60}{95} = 0,224 \text{ Vt/m} \cdot {}^\circ\text{S}$$

Thermal resistance of foam concrete:

$$R_1 = (0,016:0,224) \cdot 16 = 1,143 \text{ m}^2 \cdot {}^\circ\text{S}/\text{Vt}$$

And so:

$$R = 0,35 + 1,143 = 1,49 \text{ m}^2 \cdot {}^\circ\text{S}/\text{Vt}$$

For 48-cell foam concrete:

$$R = \frac{R_{11} + 2R_1}{3} = \frac{1,879 + 2 \cdot 1,49}{3} = 1,64 \text{ m}^2 \cdot {}^\circ\text{S}/\text{Vt}$$

In that case, the average coefficient of thermal conductivity of foam concrete:

$$\lambda_{Penobeton} = \frac{\delta}{R} = \frac{0,40}{1,64} = 0,243 \text{ Vt/m} \cdot {}^\circ\text{S}$$

**Conclusion.** The following conclusions can be made on the basis of the conducted research work:

1. The coefficient of thermal conductivity of porous foam concrete is 3-4 times smaller than the coefficient of thermal conductivity of brick.



2. The thermal resistance of foam concrete to heat transfer is 2-3 times greater than that of a brick wall with a width of 38 cm, and we can see this in the following diagram: 1 for brick, 2 for foam concrete.

## Reference

1. Madaliev, M. E. U., Maksudov, R. I., Mullaev, I. I., Abdullaev, B. K., & Haidarov, A. R. (2023). Investigation of the Influence of the Computational Grid for Turbulent Flow.
2. Akramovna, U. N., & Ismoilovich, M. R. (2021). Flow Around a Plate at Nonzero Cavitation Numbers. *Central Asian Journal of Theoretical and Applied Science*, 2(12), 142-146.
3. Muminov, O., & Maksudov, R. (2022). HIDROTECHNICS PREVENT VIBRATIONS THAT OCCUR IN CONSTRUCTIONS. *Science and innovation*, 1(A7), 762-766.
4. Maksudov, R. I., Dehqonov, S. S., & Usmonov, M. A. (2023). THERMAL INSULATION MATERIALS AND DETERMINATION OF THEIR OPTIMAL THICKNESS. *Экономика и социум*, (4-1 (107)), 151-157.
5. J Orzimatov, S Qurbanova. Using membrane ultrafiltration equipment for drinking water disinfection // Tom 1, Science and Innovation 2022/11/13
6. J.T. Orzimatov. Analysis of the prospects for the use of energy-efficient active solar devices in uzbekistan // American Journal of Applied Science and Technology, Tom 2, 2022/6/30
7. Yu K Rashidov, JT Orzimatov, K Yu Rashidov, ZX Fayziev. The method of hydraulic calculation of a heat exchange panel of a solar water-heating collector of a tube–tube type with a given nonuniform distribution of fluid flow along // Tom 56, Applied Solar Energy 2020/1
8. Yu K Rashidov, JT Orzimatov. Solar air heater with breathable matrix absorber made of metal wire tangle // Tom 5, Scientific-technical journal 2022.
9. Madaliev, E., Madaliev, M., Mullaev, I., Sattorov, A., & Ibrokhimov, A. (2023, March). Numerical simulation of the layer mixing problem based on a new two-fluid turbulence model. In *AIP Conference Proceedings* (Vol. 2612, No. 1). AIP Publishing.
10. Isroiljonovich, M. I. (2022). USE OF HEAT INSULATION MATERIALS IN HEAT NETWORKS. *CENTRAL ASIAN JOURNAL OF MATHEMATICAL THEORY AND COMPUTER SCIENCES*, 3(12), 184-189.
11. Israiljonovich, M. I. (2022). HEAT-TECHNICAL CALCULATION OF THE SOLAR COLLECTOR. *CENTRAL ASIAN JOURNAL OF MATHEMATICAL THEORY AND COMPUTER SCIENCES*, 3(12), 115-120.
12. Mullaev, I. (2022). IMPROVING THE EFFICIENCY OF THE SOLAR-AIR HEATING DEVICE. *Science and Innovation*, 1(7), 756-761.
13. Azizovich, N. I. (2022). On The Accuracy of the Finite Element Method on the Example of Problems about Natural Oscillations. *European Multidisciplinary Journal of Modern Science*, 116-124.
14. Nasirov, I. (2022). АКТУАЛЬНОСТЬ ПРИМЕНЕНИЯ МЕТОДОВ МАТЕМАТИЧЕСКОГО МОДЕЛИРОВАНИЯ И МЕТОДОВ КОНЕЧНЫХ ЭЛЕМЕНТОВ В СТРОИТЕЛЬСТВЕ. *Science and innovation*, 1(A7), 711-716.
15. Носиров, И. А. (2022). МОДЕРНИЗИРОВАНИЕ КОНСТРУКЦИЙ ТУРБОДЕФЛЕКТОРОВ. *CENTRAL ASIAN JOURNAL OF MATHEMATICAL THEORY AND COMPUTER SCIENCES*, 3(12), 126-130.



16. Nosirov, A. A., & Nasirov, I. A. (2022). Simulation of Spatial Own of Vibrations of Axisymmetric Structures. *European Multidisciplinary Journal of Modern Science*, 107-115.
17. Solijonov, M.V (2022). QUYOSH ENERGİYAsidan FOYDALANGAN YANGI QOYISH HAVO ISITISH PARAMETRLARINI ISHLAB CHIQISH PARAMETRLARINI OPTİMLAYTIRISH. *MATEMATİK NAZARIYA VA INFORMATYA FANLARI MARKAZIY ASIAN JURNALI*, 3 (12), 190-197.
18. Madraximov, M. M., Abdulkhaev, Z. E., & Ilhomjon, I. (2022). Factors Influencing Changes In The Groundwater Level In Fergana. *Int. J. Progress. Sci. Technol.*, 30, 523-526.
19. Abdulkhaev, Z., Madraximov, M., Arifjanov, A., & Tashpulotov, N. (2023, March). Optimal methods of controlling centrifugal pumps. In *AIP Conference Proceedings* (Vol. 2612, No. 1). AIP Publishing.
20. Мадхадимов, Мамадали Мамадалиевич, Зохиджон Эркинжонович Абдулхаев, and Алимардон Хамдамалиевич Сатторов. "Регулирования работы центробежных насосов с изменением частота вращения." *Актуальные научные исследования в современном мире* 12-1 (2018): 83-88.
21. Abdullayev, B. (2022). MODELING OF COLLECTOR WATER DISCHARGE INTO THE WATER COURSE IN THE FERGANA VALLEY MODELING OF COLLECTOR WATER DISCHARGE INTO THE WATER COURSE IN THE FERGANA VALLEY. *Science and innovation*, 1(A7), 827-834.
22. Qosimov A. S., Srojidinov D. R. AVTOPOEZDLAR TORMOZ MEXANIZIMLARI PNEVMATIK QUVIRLARINING TEXNIK HOLATINI, AVTOPOEZDLARNING MOS TURIGA TADBIQ QILISH //Educational Research in Universal Sciences. – 2023. – Т. 2. – №. 3. – С. 474-480.
23. Otaboyev, N. I., Qosimov, A. S. O., & Xoldorov, X. X. O. (2022). Avtopoezd tormozlanish jarayonini organish uchun avtopoezd turini tanlash. *Scientific progress*, 3(5), 87-92.
24. qizi Qurbonova, S. N. (2022). ICHIMLIK SUVLEARINI ZARARSIZLANTIRISHDA ENERGIYA TEJAMKOR TEXNOLOGIYALARDAN FOYDALANISH. *INTERNATIONAL CONFERENCE ON LEARNING AND TEACHING*, 1(8), 430-435.
25. Эгамбердиев, О. Ш., Хамдамов, А., Ўзбеков, Ж., Раҳмонқулов, С., & Халилов, Н. (2022). НАСОС СТАНЦИЯСИНИНГ ИШЛАШ ЖАРАЁНИНИ ОПТИМАЛ БОШҚАРИШ АЛГОРИТМИ. *Евразийский журнал академических исследований*, 2(11), 94-99.
26. Madaliev, M. E. U., Maksudov, R. I., Mullaev, I. I., Abdullaev, B. K., & Haidarov, A. R. (2023). Investigation of the Influence of the Computational Grid for Turbulent Flow.
27. Abdullayev, B. X., & Rahmankulov, S. A. (2021). Modeling Aeration in High Pressure Hydraulic Circulation. *Central Asian Journal of Theoretical and Applied Science*, 2(12), 127-136.
28. Abdullayev, B. X., & Rahmankulov, S. A. (2021). Movement of Variable Flow Flux Along the Path in a Closed Inclined Pipeline. *Central Asian Journal of Theoretical and Applied Science*, 2(12), 120-126.
29. Abdullayev, B. X., Xudayqulov, S. I., & Sattorov, S. M. (2020). Simulation Of Collector Water Discharges Into The Watercourse Of The Ferghana Valley. *Scientific-technical journal*, 24(3), 36-41.



30. Abdullayev, B. X., Xudayqulov, S. I., & Sattorov, S. M. (2020). Variable Flow Rate Flow Along A Path In A Closed Inclined Pipeline. *Scientific-technical journal*, 24(4), 23-28.
31. Abdujalilova, S. S., & Zukhridinovna, R. S. (2023). MEASURING WATER CONSUMPTION IN FITTINGS. *CENTRAL ASIAN JOURNAL OF MATHEMATICAL THEORY AND COMPUTER SCIENCES*, 4(5), 29-33.
32. Рашидов, Ю. К., Орзиматов, Ж. Т., Эсонов, О. О. Ў., & Зайнабидинова, М. И. К. (2022). Солнечный воздухонагреватель с воздухопроницаемым матричным абсорбером. *Scientific progress*, 3(4), 1237-1244.
33. Esonov, O., Abdullayeva, G., & Obidxo'Jayev, J. (2022). INCREASE THE EFFICIENCY OF SOLAR WATER COLLECTORS. *Science and innovation*, 1(A7), 785-789.
34. Rashidov, Y. K., & Orzimatov, J. T. (2022). SOLAR AIR HEATER WITH BREATHABLE MATRIX ABSORBER MADE OF METAL WIRE TANGLE. *Scientific-technical journal*, 5(1), 7-13.
35. qizi Tillaboyeva, F. S. (2023). QUYOSHLI SUV ISITGICH KOLLEKTORLARINING ISSIQLIK ALMASHINUVI HISOBI. GOLDEN BRAIN, 1(31), 156-162.
36. qizi Tillaboyeva, F. S. (2022). QUYOSH KOLLEKTORLARI. QUYOSH KOLLEKTORLARINING TURLARI VA KOMPONENTLARI. *INTERNATIONAL CONFERENCE ON LEARNING AND TEACHING*, 1(6), 255-258.
37. Maksudov, RI, Dehkanov, SS, & Usmanov, MA (2023). THERMAL INSULATION MATERIALS AND DETERMINATION OF THEIR OPTIMAL THICKNESS. *Economics and society* , (4-1 (107)), 151-157.
38. Madaliyev, E., & Maksitaliyev , B. (2022). A NEW WAY OF GETTING ELECTRICITY. *Science oath innovation* , 1 (A7), 790-795.
39. Solijonov, MV (2022). QUYOSH ENERGIYAsidan FOYDALANGAN YANGI QOYISH HAVO ISITISH PARAMETRLARINI ISHLAB CHIQISH PARAMETRLARINI OPTIMLAYTIRISH. *MATEMATİK NAZARIYA VA INFORMATYA FANLARI MARKAZIY ASIAN JURNALI* , 3 (12), 190-197.
40. Abdurakov, BA, Solijonov, MV, & Abdumalikov, RR (2023). AN'VANSIY VA QAYTA OLiladigan ENERGIYA MANBALARI ASOSIDA ISHLAB CHIQISH ISILIK TA'MINLANISH TIZIMLARINI TADQIQOT. *OLTIN MIYA* , 1 (1), 253-255.